

HAWCStab2 User Manual



November 2017

DTU Wind Energy Department of Wind Energy



Author(s): Morten Hartvig Hansen, Lars Christian Henriksen, Carlo Tibaldi, Leonardo Bergami, David Verelst, Georg Pirrung
Title: HAWCStab2: User Manual
Institute: Department of Wind Energy

Summary (max. 2000 char.):

This report is a user manual for the code HAWCStab2. HAWCStab2 is an implementation of an analytical linearization of a nonlinear finite beam element model. The beam model is coupled with an unsteady blade element momentum model of the blade aerodynamics. The aerodynamic model includes shed vorticity, dynamic stall, and dynamic inflow. The code allows for steady-states computations and open-loop and closed-loop modal analysis. Publication Date: October 2017

HAWCStab2 version: 2.14

E-mail: hawcstab2@vindenergi.dtu.dk

Web-page: www.hawcstab2.vindenergi.dtu.dk

Address: Technical University of Denmark DTU Wind Energy Frederiksborgvej 399 4000 Roskilde Denmark

Preface

This report is the user manual of HAWCStab2. HAWCStab2 was originally developed by Morten Hartvig Hansen. HAWCStab2 is a frequency based aeroservoelastic code for steady states computation and stability analysis of wind turbines. The code, to some extent, reads the same input files as HAWC2. HAWCStab2 is available in three versions: HAWCStab2, which is graphical user interface based program, HAWC2S, which is a command line based program suitable for e.g. optimization, and HS2pid, which is another command line program, is available with reduced functionality. HS2pid is only able to calculate tuning parameters for the Basic DTU Wind Energy Controller assuming torsionally stiff blades. HAWCStab2 is, so far, only able to handle 3 bladed wind turbines.

Contents

1.	Introduction	6
2.	Input file and commands 2.1. HAWC2 commands 2.1.1. new_htc_structure 2.1.2. wind 2.1.3. aero 2.1.4. MWCStab2 commands 2.2.1. Structural setup 2.2.2. Damping 2.2.3. Operational data 2.2.4. Controller tuning 2.2.5. Controller input/output 2.2.6. HAWC2S commands 2.2.7. Advanced options	7 7 8 8 9 9 10 11 13 13 15 18 20
3.	Output files 3.1. Operational data in .opt 3.2. Performance data in .pwr 3.3. Spanwise steady-state results in .ind 3.4. Frequencies and damping ratios in .cmb 3.5. System matrices 3.5.1. Structural matrices 3.5.2. Open-loop matrices 3.5.3. Closed-loop matrices	21 21 21 22 25 26 26 26 26 27
4.	Examples 4.1. Examples with the GUI: HAWCStab2.exe 4.1.1. Calculating operational points 4.1.2. Calculating steady state and induction 4.1.3. Performing open-loop aeroelastic modal analysis 4.1.4. Tuning of PI controller 4.1.5. Performing closed-loop aeroelastic modal analysis 4.2. Examples with the command line program: HS2pid.exe	 28 28 30 31 32 32 34
5.	Keyboard shortcuts	35
Α.	GnuPlot files	36

1. Introduction

HAWCStab2 is a tool developed at the Department of Wind Energy of the Technical University of Denmark. HAWCStab2 is an improved version of HAWCStab [1] with a different kinematic. The model is an analytical linearization of a nonlinear finite beam element model. The beam model is coupled with an unsteady blade element momentum model of the blade aerodynamic. The aerodynamic model includes shed vorticity, dynamic stall, and dynamic inflow. Hansen [2] gives a detailed description of the model. A validation and analysis of the open-loop performances are provided by Sønderby and Hansen [3]. An analysis in closed-loop is shown by Tibaldi et al. [7].

In Chapter 2 the basic structure of the htc file is explained. In Chapter 3 the output files are explained. In Chapter 4 a few examples on how to use the program are shown.

The examples shown in this document are based on:

- HAWC2 (version 11.8)
- HAWCStab2 (version 2.14)
- DTU 10MW RWT (version 2.0)

2. Input file and commands

The input to HAWCStab2 is an htc-file, which is also used for HAWC2. The file used by HAWCStab2 has the normal HAWC2 specific commands as well as some HAWCStab2 specific commands.

2.1. HAWC2 commands

The following subsections give a short descriptions of the HAWC2 input required by HAWCStab2. The HAWC2 user manual [4] available at www.hawc2.dk should be consulted for a detailed description of the commands.

The following sections describe the HAWC2 blocks of the htc file are used by HAWCStab2. Other blocks such as e.g. **simulation**, **aerodrag**,**force**, **hydro**, **soil**, **dll** and outputs are not used by HAWCStab2.

2.1.1. new_htc_structure

The **new_htc_structure** block defines the structural setup of the wind turbine. Herein, it defines the various main bodies e.g. *tower*, *towertop*, *shaft*, *hub* and *blade* in the **main_body** sub block. The main orientation of the main bodies is then defined in then **orientation** sub block. The interconnection of the main bodies is defined in the **constraints** sub block.

```
begin new_htc_structure;
  begin main_body;
  ...
  end main_body;
;
  begin orientation;
  ...
  end orientation;
;
  begin constraint;
  ...
  end constraint;
end new_htc_structure;
```

Constraints The bottom of the first main body defined in the HAWCStab2 substructure **ground_fixed_substructure** (see Section 2.2.1) is always fixed to the ground. The remaining constraints between the main bodies will follow the HAWC2 commands with the exception of the shaft bearing.

Two different types of bearing constraints are basically available in HAWCStab2: **bearing1** and **bearing2**. The first type of bearing allows free rotation about one axis. This bearing is normally used for the shaft. A **bearing2** allows for a rotation about one axis where the angle is set from an input to the system. This type of bearing is normally used for the pitch bearing of pitch regulated wind turbines.

Note that if the user specifies a **fix1**, **bearing2** or **bearing3** for the constraint between the last main body of the HAWCStab2 substructures **ground_fixed_substructure** and **rotating_axissym_substructure**, then this bearing constraint will be treated as a constant speed bearing (the **omegas** input is ignored in case of a the **bearing3** command) and there is no generator rotation degree of freedom.

2.1.2. wind

The **wind** block contains information about *density* of air, which is only parameter used by HAWCStab2.

```
begin wind ;
```

```
density
                          1.225 ;
 wsp
                          11
                          0.201454545454545
 tint
                                               ;
 horizontal_input
                          1
                               ;
                                              0=false, 1=true
                                         yaw, tilt, rotation
 windfield_rotations
                          0 0.0 0.0 ;
                          0.0 0.0 -119.00 ; hub height
 center_pos0
                          3 0.2 ;
 shear_format
 turb_format
                          0
                               ; 0=none, 1=mann,2=flex
 tower_shadow_method
                          0
                               ; 0=none, 1=potential flow, 2=jet
end wind;
```

2.1.3. aero

The **aero** block contains information about aerodynamic properties for the blade such drag and lift coefficients. Furthermore, *induction_method* and *tiploss_method* are used by HAWCStab2.

```
begin aero ;
  nblades 3;
  hub_vec shaft -3 ;
  link 1 mbdy_c2_def blade1;
  link 2 mbdy_c2_def blade2;
  link 3 mbdy_c2_def blade3;
```

ae_filename	./data/DTU_10MW_RWT_ae.dat ;
pc_filename	./data/DTU_10MW_RWT_pc.dat ;
induction_method	1 ; 0=none, 1=normal
aerocalc_method	1 ; 0=ingen aerodynamic, 1=med aerodynamic
aerosections	50 ;
ae_sets	1 1 1;
tiploss_method	1 ; 0=none, 1=prandtl
dynstall_method	2 ; 0=none, 1=stig oye method,2=mhh method
end aero ;	

2.2. HAWCStab2 commands

HAWCStab2 needs a specific block called **hawcstab2**. Within this block different commands are specified, which can be divided into the following inputs:

- structural setup
- damping
- operational data
- controller tuning
- controller input/output
- HAWC2s specific commands
- advanced options

All of these inputs are explained in the following sections.

2.2.1. Structural setup

The structural setup is specified through three different blocks where the bodies are listed:

- **ground_fixed_substructure**: main bodies that are fixed with respect to the ground, e.g. tower, and tower top;
- **rotating_axissym_substructure**: rotating main bodies that are not part of the rotor, e.g. shaft. These bodies have to be axis-symmetric;
- **rotating_threebladed_substructure**: rotating main bodies that are part of the rotor, e.g. hub and blades. Since HAWCStab2 assumes 3 bladed with isotropic rotor, only the first blade and hub bodies need to be specified, the others will be included automatically.

A second-order model of a pitch actuator can also be included in the wind turbine model. The model is included adding the line

second_order_actuator pitch1 100.0 0.7 ;

in the block **rotating_threebladed_substructure**. The first number in the command indicates the frequency of the second-order model, the second its damping ratio.

All the aerodynamic forces are assumed to be applied on the last main body in the block rotating_threebladed_substructure.

The format of these commands is:

```
begin hawcstab2 ;
begin ground_fixed_substructure ;
main_body tower ;
main_body towertop ;
end ground_fixed_substructure ;
begin rotating_axissym_substructure ;
main_body shaft ;
end rotating_axissym_substructure ;
begin rotating_threebladed_substructure ;
main_body hub1 ;
main_body blade1 ;
second_order_actuator pitch1 100.0 0.7 ;
end rotating_threebladed_substructure ;
end hawcstab2 ;
```

2.2.2. Damping

If *log_decrements* is present in the block of either **ground_fixed_substructure**, **rotating_axissym_substructure** or **rotating_threebladed_substructure** then the HAWC2 specific damping commands will be overwritten by a spectral damping model will be used to calculate the damping properties. If for example the following command is present in the **rotating_threebladed_substructure**:

log_decrements 1.0 1.2 1.5 2.0 ;

then the first four modes of the unloaded blade are structurally damped 1.0%, 1.2%, 1.5%, and 2.0%. The logarithmic decrements of higher order modes will be increased relatively with the factor 1.1 until a hard-coded maximum of 70%.

If *log_decrements* is not used then the Rayleigh type damping model of HAWC2 will be used. The damping properties will be calculated for the unloaded, standstill wind turbine. It is strongly recommended only to use stiffness proportional terms. If mass proportional terms are used, the damping for HAWC2 and HAWCStab2 will not be the same. Consult Hansen [5] for more information about the mixed mass/stiffness damping model.

2.2.3. Operational data

The **operational_data** block is optional. It is used to set the default values of the parameters in the dialog window to compute the operational data points and to set the values when running with HAWC2S. The parameters of this block are:

- windspeed, the minimum wind speed value, the maximum wind speed value, and the number of wind speed between the minimum and maximum.
- genspeed, the minimum rotational speed, and the maximum rotational speed in rpm.
- gearratio and the gear ratio.
- minpitch and the minimum pitch angle in degree.
- opt_lambda and the value of the tip-speed-ratio for the variable speed region.
- maxpow and the value of the aerodynamic rated power in kW.
- prvs_turbine and an integer to indicate the type of pitch regulation. 0 for fixed pitch and 1 for variable pitch.
- include_torsiondeform and an integer to indicate if blade deformations should be included in the computation. 0 for no deformations and 1 for with deformations.

If the operational data points have been precomputed or the user wants to enter them manually, it is possible to specify them through a file. The file is specified by the command:

operational_data_filename ./operational_data_filename.opt ;

When given as input the file requires three columns: one for the wind speed, one for the pitch angle and one for the rotor speed. The number of data points included in the file need to be specified in the first row of the file. When the file is saved from HAWCStab2 it adds two extra columns containing the aerodynamic power and thrust. These last two columns are not needed as inputs because HAWCStab2 is used to compute them.

Aero thrust [kN]	224.286816	352.209828	500.388658	658.232557	816.795864	1034.430140	1277.059791	1544.121977	1262.557036	1080.883000	970.253169	892.739336	828.619150	780.318935	740.590975	706.090035	677.263923	651.469908	630.689690	610.636055	594.608862	580.889756
Aero power [kW]	287.319260	805.573745	1543.002742	2525.245528	3770.277010	5374.530562	7378.855371	9826.489718	10636.875545	10640.312112	10634.865878	10652.538640	10618.567809	10631.933899	10646.833268	10640.981055	10646.834596	10632.078861	10648.917163	10622.019335	10628.972396	10638.692060
Rot. speed [rpm]	6.00000	6.00000	6.00000	6.00000	6.424607	7.226938	8.031337	8.839966	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000	9.600000
Pitch [deg]	2.889748	2.115800	1.109058	0.000048	0.000055	0.000019	0.000056	0.000048	4.807932	7.388350	9.289680	10.887191	12.346992	13.672693	14.926127	16.120324	17.268079	18.374175	19.443877	20.484638	21.496839	22.485124
22 Wind speed [m/s]	4.000000	5.000000	6.000000	7.000000	8.000000	9.000000	10.000000	11.000000	12.000000	13.00000	14.00000	15.00000	16.00000	17.000000	18.00000	19.00000	20.000000	21.000000	22.000000	23.00000	24.000000	25.000000

The operational_data_filename file contains information about the operational points for selected wind speeds.

2.2.4. Controller tuning

This section contains two main commands. A command to set the parameters to automatically compute the tuning of the controller and a command to manually specify the controller tuning.

The controller_tuning block is optional, see 4.1.4 for an example. It is used to set the default values of the parameters in the dialog window to tune the controller and to set the values when running with HAWC2S. The parameters of this block are:

- partial_load, the frequency [Hz], and damping ratio [-] of the regulator mode. These vales are used for the pole placement of the PI controller on the generator torque in partial load region.
- full_load, the frequency [Hz], and damping ratio [-] of the regulator mode. These vales are used for the pole placement of the PI controller on the pitch in full load region.
- gain_scheduling and an integer to specify the type of gain scheduling. 1 for linear and 2 for quadratic.
- constant_power and an integer to specify if the regulator strategy is constant torque 0 or constant power 1.
- rotorspeed_gs and an integer to specify if the gain scheduling should contain also a term due to the aerodynamic damping 0 or 1.
- **regions** and four integers to specify the operational points at which there is a transition in the controller operational regions. This command is optional and overwrites the build-in function that identifies the operational regions.

Two different controllers can be added to the model through the following commands:

- basic_dtu_we_controller (# 1)
- pi_pitch_controller (# 2)

The first controller is a simplified linearization of the Basic DTU Wind Energy controller, so it includes sub-controllers to handle the different operational regions. The second controller is only meant for the full load region and it is a basic PI pitch controller. Both commands require several tuning parameters. The parameters are described in Table 2.1.

2.2.5. Controller input/output

This section specifies the input and outputs to the wind turbine models. These are used to compute the input and output matrices. The inputs and outputs are specified following the outputs convention of HAWC2. An example is:

#1	# 2	Parameter	Unit	Description
	1	P_rated	kW	Rated power.
	2	Omega_rated	rad/s	Rated rotor rotational speed.
1		Kp_partial		Prop. gain of partial load PI torque con- troller.
2		Ki_partial		Int. gain of partial load PI torque controller.
3		Kopt_partial		K-omega control parameter.
4	3	Kp_full		Prop. gain of full load PI pitch controller.
5	4	Ki_full		Int. gain of full load PI pitch controller.
6	5	K1_theta		Gain scheduling parameter of the full load PI gains w r t_ pitch angle
7	6	K2_theta		Gain scheduling parameter of the full load PI gains w.r.t. pitch angle.
8	7	omega_filt		Natural frequency of second order speed fil- ter.
9	8	csi_filt		Damping ratio of second order speed filter.
10		DT_freq		Frequency of a band-stop filter to remove the drivetrain frequencies.
11	9	type		Full load generator control type: 1 constant power, 0 constant torque.
12	10	KO_omega		(Optional) Gain scheduling of the full load PI gains w.r.t. rotor speed.
13	11	K1_omega		(Optional) Gain scheduling of the full load PI gains w.r.t. rotor speed.
14	12	K2_omega		(Optional) Gain scheduling of the full load PI gains w.r.t. rotor speed.

Table 2.1.: Parameters for build-in controller commands.

```
begin controller ;
begin input ;
constraint bearing1 shaft_rot ;
constraint bearing2 pitch1 collective ;
end input ;
begin output ;
constraint bearing1 shaft_rot 1 only 2 ;
constraint bearing2 pitch1 1 only 1 collective ;
mbdy momentvec tower 1 2 tower ;
end output ;
end controller ;
```

2.2.6. HAWC2S commands

HAWC2S is the command line version of HAWCStab2. The input file for HAWC2S must contain all the parts used in the input file for HAWCStab2.

When using HAWC2S, the commands, that are selected through the GUI interface in HAWCStab2, must be included in the htc file as command lines. These are then executed as a workflow. The commands have to be inserted in the hawcstab2 section.

For some commands an output file is generated and the file name is derived from the used htc input file, and which is represented here conceptually as: input_htc_file.ext. The new output is then converted to the following format: input_htc_file_APPENDIX.NEW_EXT, where _APPENDIX is used for some of the output commands but not all (see below for more details), and depends on the analysis executed prior to save command. The file extension is replaced with an appropriate alternative NEW_EXT for each of the different commands.

The commands available are:

- compute_optimal_pitch_angle use_operational_data
 - will compute and save to a file the operational data points according to the parameters inserted in the operational_data block. The rotor rotational speed is computed according to the user-defined tip-speed-ratio and the minimum and maximum rotor speeds. The pitch angle at each operational point is computed to maximize the aerodynamic torque or to guarantee the user-defined rated power value.
- compute_structural_modal_analysis Parameters:
 - bladeonly or nobladeonly to specify if the analysis is for the blade only or for the whole wind turbine.
 - an integer to specify the number of modes.

Results saved to file:

- input_htc_file_Blade_struc.cmb for a structural blade-only analysis.
- input_htc_file_struc.cmb for a structural system analysis

• compute_steady_states - (Sec. 4.1.2)

to compute the steady states from given operational points. The command needs four parameters

- bladedeform or nobladedeform to specify if blade deformations needs to be included in the computations.
- tipcorrect or notipcorrect to specify if tip correction needs to be included in the computations.
- induction or noinduction to specify if induction needs to be included in the computations.
- gradients or nogradients to specify if gradients needs to be computed. The gradients are then printed in the .pwr file.
- compute_stability_analysis[§] (Sec. 4.1.3) Parameters:
 - bladeonly or windturbine
 - an integer to specify the number of modes.

Results saved to file:

- input_htc_file_Blade.cmb for a blade-only aeroelastic analysis.
- input_htc_file.cmb for a system aeroelastic analysis.

compute_aeroservoelastic[§]
 Parameters:

- an integer to specify the number of modes.

Results saved to file:

- input_htc_file_Servo.cmb
- save_ol_matrices[§] Writes out the open-loop A,B,C,D matrices to text files.
- save_ol_matrices_full[§] Writes out the M,D,K matrices to text files.
- save_ol_matrices_all[§] Writes out both A,B,C,D and M,D,K matrices to text files.
- save_cl_matrices_all[§] Writes out the closed-loop A, B, Bv, C, D, Dv, E, F, Fv matrices to text files.

This command needs the block **controller**. Beside the specified closed-loop aeroservo-elastic matrices, additional matrices can be saved by specifying *one* of the following additional arguments:

- ctrl_out Saves also the controller matrices, Ac, Bc, Cc, Dc.
- vloc_out Saves also the local wind matrices, Bv loc, Dv loc, Fv loc
- ctrl_vloc_out Saves both the controller matrices and the local wind ones.

• compute_controller_input[§] (Sec. 4.1.4)

This command needs the block controller. Optional parameter:

- outputfile.txt, defaults to input_htc_file_ctrl_tuning.txt.
- save_power[§]

Results saved to file: input_htc_file.pwr.

• save_induction[§]

For each operating point three files are saved, and each operating point contains the used wind speed as a reference WSP=int(windspeed*1000):

- input_htc_file_uWSP.ind
- input_htc_file_fext_uWSP.ind
- input_htc_file_defl_uWSP.ind

• degrees_of_freedom

Lock different degrees of freedom and select the inflow model. Parameters:

- true or false to specify if the ground fixed substructure is rigid
- true or false to specify if the rotating axial symmetric substructure is rigid
- true or false to specify if the rotating three bladed substructure is rigid
- true or false to set quasi-steady aerodynamic
- frozen, quasi or dynamic to indicate the desired type of inflow.
- save_beam_data
- save_blade_geometry
- save_aero_point_data
- save_profile_coeffs
- save_modal_amplitude Save modal amplitudes to file: input_htc_file_APPENDIX.amp as follows:
 - input_htc_file_Blade_struc.amp for a structural blade-only analysis.
 - input_htc_file_struc.amp for a structural system analysis
 - input_htc_file_Blade.amp for a blade-only aeroelastic analysis.
 - input_htc_file.amp for a system aeroelastic analysis.
 - input_htc_file_Servo.amp for an aero-servo-elastic analysis
- save_modal_binary

Save modal results in binary format to file: input_htc_file_APPENDIX.NEW_EXT as follows:

- input_htc_file_Blade_struc_Modal.hmd for a structural blade-only analysis.
- input_htc_file_struc_Modal.hmd for a structural system analysis

- input_htc_file_Blade_Modal.hsd for a blade-only aeroelastic analysis.
- input_htc_file_Modal.hsd for a system aeroelastic analysis.
- input_htc_file_Servo_Modal.hsd for an aero-servo-elastic analysis
- save_eigenvalues

Save eigenvalues to file: input_htc_file_APPENDIX.dat as follows:

- input_htc_file_Blade_struc.dat for a structural blade-only analysis.
- input_htc_file_struc.dat for a structural system analysis
- input_htc_file_Blade.dat for a blade-only aeroelastic analysis.
- input_htc_file.dat for a system aeroelastic analysis.
- input_htc_file_Servo.dat for an aero-servo-elastic analysis

The commands with the symbol \S require the commands <code>compute_steady_states</code> to be executed first.

2.2.7. Advanced options

Advanced options commands can be entered as HAWC2S commands but will be executed also with HAWCStab2.

• verbose

This command prints additional information in the log files.

steady_state_convergence_limits

Modify the convergence criterion for the computation of the operational points and steady states. The command is followed by a sequence of nine parameters. The parameters and their default values when the command is not issued are:

- 1. Absolute tolerance on the 2-norm of the change of induction factors in each aerodynamic section, default=1e-6
- 2. Maximum number of BEM iterations in a single aerodynamic section, default=10000
- 3. Relaxation factor of the BEM iterations (low number is stable but slower), default=0.02
- 4. Relative tolerance on the force differences in the inner and outer iteration loops (see Figure 2.1), default=1e-5
- 5. Maximum number of iterations in either the inner or outer iteration loop, default=500
- 6. Relaxation factor of the increment of the blade deformation, default=0

- 7. Maximum variation of operating point characteristic in compute optimal operation data (e.g. pitch angle above rated), default=10.0. The variation is given with respect to the previously computed value, or to zero for the first point; hence this value should be increased when computing operational data at a single operating point above rated.
- 8. Maximum variation of operating point characteristic between stiff computations and computations with blade deformation in compute optimal operation data. The default value 5.0 can be decreased for wind turbines that are not very flexible.
- 9. Absolute tolerance on pitch angle for the optimal operational point computations, default=1e-9.

Example:

```
steady_state_convergence_limits 1e-7 1e4 0.02 1e-6 1e3 0 10.0 5.0 1e-9
```

Figure 2.1 shows a representation of the iterative process to obtain the nonlinear steady-states solution. Two loops can be identified: an outer loop where the aerodynamic forces are calculated with the BEM and an inner loop where the deflections are computed for fixed forces. Both loops these use the aeroelastic convergence parameters (4, 5, and 6). Their absolute tolerances are computed from the relative tolerance (denoted ϵ_{rel}) as $\epsilon_i = \epsilon_o = 150\epsilon_{rel}S_o$, where S_o is the blade curve length.

• print_full_precision

Save operational points file with extended precision.



Figure 2.1.: Diagram representing the iterative process to obtain the nonlinear steadystates solution.

2.3. Automatic mode sorting

Since version 2.14, HAWCStab2 and HAWC2S have an automatic mode sorting algorithm that does not require any other input from the user than the number of desired modes. The modes are the eigensolutions most similar to the structural modes. Thus, the openor closed-loop aeroelastic modes sorted out are only the modes that have a mode shape similar to the structural modes. This algorithm removes eigensolutions dominated by state variables of the unsteady aerodynamic models or the controller equations. Note that the user can change the number of modes to be plotted and saved under the menu **Plot**.

3. Output files

This chapter describes some of the output files that can be generated with HAWCStab2. When saving result files, extensions must be added in the file name. It is an advantage to use the extensions suggested in the dialog window because the already existing files of similar format are then filtered out.

3.1. Operational data in .opt

The operational data file is an input/output file. To perform steady-states computations a set of operational points is required, and these are passed to HAWCStab2 with an .opt file. This file can be generated by HAWCStab2 with the commands Optimal operational data plus Save optimal power data. When saved, the file contains five columns, each column correspond to:

- 1. Wind speed [m/s]
- 2. Pitch angle [deg]
- 3. Rotor speed [rpm]
- 4. Aerodynamic power [kW]
- 5. Aerodynamic thrust [kN]

When the file is used as input, it can be arbitrary modified by the user, i.e., any operational point can be given as an input. Because an operational point is defined uniquely by wind speed, pitch angle, and rotor speed only the first three columns need to be present in the file, all the other columns are not read. Special attention need to be paid to the first line of the file because it contains a number. This number needs to be equivalent to the number of operational points included in the file.

3.2. Performance data in .pwr

This file is generated with the command **save power**. In the file each row corresponds to an operational point and each column refers to a parameter or computed result as follows:

#	Name	Description
1	V	Wind speed [m/s]
2	Р	Aerodynamic power [kW]
3	Т	Aerodynamic thrust [KN]
4	Ср	Power coefficient [-]
5	Ct	Thrust coefficient [-]
6	Pitch Q	Pitch torque [kNm]
7	Flap M	Hub root out-of-plane bending moment [kNm]
8	Edge M	Hub root in-plane bending moment [kNm]
9	Pitch	Pitch angle [deg]
10	Speed	Rotor speed [rpm]
11	Tip x	In-plane tip position relative to the rotor center [m]
12	Тір у	Out-of-plane tip position relative to the rotor center [m]
13	Tip z	Radial tip position relative to the rotor center [m]
14	J_rot	Rotor inertia $[\text{kg m}^2]$
15	J_DT	Inertia of entire drivetrain including rotor $[\text{kg m}^2]$
16^{*}	dQ/dt	Wake updated: Aero. torque gain of pitch angle change $[kNm/deg]$
17^*	dQ/dV	Wake updated: Aero. torque gain of wind speed change [kNs]
18^*	dQ/dO	Wake updated: Aero. torque gain of rotor speed change [kN-
		m/rpm]
19^{*}	dT/dt	Wake updated: Aero. thrust gain of pitch angle change $[kN/deg]$
20^{*}	dT/dV	Wake updated: Aero. thrust gain of wind speed change [kNs/m]
21^{*}	dT/dO	Wake updated: Aero. thrust gain of rotor speed change [kN/rpm]
22^{*}	dQ/dt	Frozen wake: Aero. torque gain of pitch angle change [kNm/deg]
23^{*}	dQ/dV	Frozen wake: Aero. torque gain of wind speed change [kNs]
24^{*}	dQ/dO	Frozen wake: Aero. torque gain of rotor speed change [kNm/rpm]
25^*	dT/dt	Frozen wake: Aero. thrust gain of pitch angle change [kN/deg]
26^*	dT/dV	Frozen wake: Aero. thrust gain of wind speed change [kNs/m]
27^{*}	dT/dO	Frozen wake: Aero. thrust gain of rotor speed change [kN/rpm]

The derivatives marked by * are only saved if the option to compute the aerodynamic gradients is selected in the dialog window of the computation of the steady states. The gradients are either assuming an instantly updated wake corresponding the gradients on the CP and CT surfaces, or assuming frozen wake where the induced velocities are kept constant.

3.3. Spanwise steady-state results in .ind

This file is generated with the command save steady state. One file for each operational point is saved. The files contain a matrix where each row corresponds to a spanwise aerodynamic station on the last main body of the **rotating_threebladed_substructure**. The columns are

#	Name	Description
1	s [m]	Curvilinear coordinate
2	A [-]	Axial induction factor
3	AP [-]	Tangential induction factor
4	PHI0 [rad]	Inflow angle in rotor plane coordinates
5	ALPHA0 [rad]	Angle of attack
6	U0 [m/s]	Relative wind speed
7	FX0 [N/m]	Force in rotor plane coordinates (in-plane)
8	FY0 [N/m]	Force in rotor plane coordinates (out-of-plane)
9	M0 [Nm/m]	Moment in rotor plane coordinates
10	UX0 [m]	In-plane deflection of aero. center relative to rotor center
11	UY0 [m]	Out-of-plane deflection of aero. center relative to rotor center
12	UZ0 [m]	Radial deflection of aero. center relative to rotor center
13	Twist [rad]	Static chord twist including pitch
14	X_AC0 [m]	In-plane position of aero. center relative to rotor center
15	Y_AC0 [m]	Out-of-plane position of aero. center relative to rotor center
16	Z_AC0 [m]	Radial position of aero. center relative to rotor center
17	CL0 [-]	Lift coefficient
18	CD0 [-]	Drag coefficient
19	CM0 [-]	Moment coefficient
20	CLp0 [1/rad]	Slope of lift coefficient
21	CDp0 [1/rad]	Slope of drag coefficient
22	CMp0 [1/rad]	Slope of moment coefficient
23	F0 [-]	Steady value of the separation function
24	F'[1/rad]	Slope of the separation function
25	CL_FS0 [-]	Lift coefficient of the fully separated lift curve
26	CLFS'[1/rad]	Slope of the fully separated lift coefficient
27	$V_a [m/s]$	Axial induced velocity
28	$V_{t} [m/s]$	Tangential induced velocity
29	Tors. [rad]	Torsional component of chord rotation (here torsional refers to
		rotation about the spanwise unit-vector of the chord coordinate
		system of the undeformed blade.
20	vx [m/s]	Relative inflow in chord reference system (chordwise)
31	vy [m/s]	Relative inflow in chord reference system (normal)
32	chord [m]	Chord
33	CT [-]	Thrust coefficient
34	CP [-]	Power coefficient
35	angle [rad]	Angle describing together with columns 36–38 the complete rota-
		tion of the chord coordinate system from the undeformed blade
36	v1 [-]	In-plane vector comp. related to the rotation angle in column 35
37	v2 [-]	Out-of-plane vector comp. related to the rot. angle in column 35
38	v3 [-]	Radial vector comp. related to the rotation angle in column 35

Additional files with <u>_fext</u> inserted in the file names are also saved with the extension .ind. These files contain the spanwise distributions of the structural forces and moments on the last main body of the **rotating_threebladed_substructure**. The columns are

#	Name	Description
1	s [m]	Curvilinear coordinate
2	Node [-]	Node number (node 1 is the blade flange)
3	$Fx_e [N]$	Edgewise force in element coordinates
4	$Fy_e [N]$	Flapwise force in element coordinates
5	$Fz_e [N]$	Spanwise force in element coordinates
6	Mx_e [Nm]	Edgewise moment in element coordinates
$\overline{7}$	My_e [Nm]	Flapwise moment in element coordinates
8	Mz_e [Nm]	Torsional moment in element coordinates
9	$Fx_r [N]$	Edgewise force in rotor coordinates
10	Fy_r [N]	Flapwise force in rotor coordinates
11	Fz_r [N]	Spanwise force in rotor coordinates
12	Mx_r [Nm]	Edgewise moment in rotor coordinates
13	My_r [Nm]	Flapwise moment in rotor coordinates
14	Mz_r [Nm]	Torsional moment in rotor coordinates

Additional files with _defl_u inserted in the file names are also saved with the extension .ind. These files contain the spanwise distributions of the nodal positions and deformations of the elements on the last main body of the rotating_threebladed_substructure. The columns are

#	Name	Description
1	s [m]	Curvilinear coordinate
2	Element no [-]	Element number
3	$pos_{xR} [m]$	In-plane position of element origo relative to the blade flange
		(origo)
4	$pos_yR [m]$	Out-of-plane position of element origo relative to the blade
		flange (origo)
5	$pos_z R [m]$	Radial position of element origo relative to the blade flange
		(origo)
6	Elem angle [rad]	Angle describing together with columns 7–9 the complete ro-
		tation of the element coordinate system from the undeformed
		blade
7	Elem v_1 $[-]$	In-plane vector comp. related to the rotation angle in column
		6
8	Elem v_2 $[-]$	Out-of-plane vector comp. related to the rot. angle in column
		6
9	Elem v_3 $[-]$	Radial vector comp. related to the rotation angle in column 6
10	Node 1 angle [rad]	Angle describing together with columns 11–13 the complete
		rotation of the first element node relative to the element coor-
		dinate system
11	Node 1 v_1 $[-]$	In-plane vector comp. related to the rotation angle in column
10		10
12	Node 1 v_2 $[-]$	Out-of-plane vector comp. related to the rot. angle in column
10		
13	Node I v_3 [-]	Radial vector comp. related to the rotation angle in column 10
14	Node 2 angle [rad]	Angle describing together with columns 15–17 the complete
		rotation of the second element node relative to the element
15	N-d-91[]	coordinate system
15	Node 2 V_{-1} [-]	In-plane vector comp. related to the rotation angle in column
16	Nodo 9 - 9 []	14 Out of plane water comp. related to the net, angle in column.
10	Node $Z V_Z [-]$	Out-of-plane vector comp. related to the rot. angle in column 14
17	Nodo 2 v 3 []	Padial vector comp_related to the rotation angle in column 14
18	Florention $[m]$	Flongation of the element
10	Enougation [m]	Enougation of the element

3.4. Frequencies and damping ratios in .cmb

The files with these extensions can contain results form eigenvalues analysis. Depending on what the user selects these results can be from structural analysis, open-loop analysis, and closed-loop analysis. In the file each line refers to an operational point.

For the structural eigenanalysis there are 1+2N columns, where N refers to the number of modes. The first column refers to the wind speed, the following N columns refer to the damped frequencies of the modes and the last N columns refer to the respective damping. Hence if the user selects to compute 15 modes, with the command

aeroelastic modal analysis, and then saves the file, with the command save frequencies and dampi the file will contain 31 columns.

In case of an aero- or aeroservo-elastic analysis, an additional N columns are added (after the 1+2N columns for frequencies and damping) referring to the real part of the eigenvalue of each respective mode. As a result, the output file will now contain 1+3N columns.

3.5. System matrices

When saving the system matrices the following files are generated, depending on the command selected.

3.5.1. Structural matrices

- tm_mat Structural mass matrix.
- tc_mat Damping matrix.
- tk_mat Stiffness matrix.
- phi_mat Transformation matrix to reduce the system.
- vtmtotv Reduced structural mass matrix.
- vtctotv Reduced structural damping matrix.
- vtktotv Reduced structural stiffness matrix.

3.5.2. Open-loop matrices

Corresponding to the state and output equation:

$$\begin{cases} \dot{x} = Ax + Bu + B_V w\\ y = Cx + Du + D_V w \end{cases}$$
(3.1)

- amat Open-loop A matrix.
- bmat Open-loop B matrix, input from the controller.
- cmat Open-loop C matrix.
- dmat Open-loop D matrix, input from the controller.
- bvmat Open-loop B matrix, input from uniform wind in three components, collective, cosine, and sine.
- dvmat Open-loop D matrix, input from uniform wind.
- bvmat_loc_v Open-loop B matrix, input from wind at each aerodynamic section along the blade in three components, collective, cosine, and sine.

- dvmat_loc_v Open-loop D matrix, input from wind at each aerodynamic section along the blade in three components, collective, cosine, and sine.
- gmat
- gvmat
- gvmat_loc_v

3.5.3. Closed-loop matrices

Corresponding to the state and output equation:

$$\begin{cases} \dot{x} = Ax + Bu_{\text{pert}} + B_V w \\ y = \left[z_{\text{ctrl}}^T, u_{\text{ctrl}}^T \right]^T = Cx + Du_{\text{pert}} + D_V w \\ z_{\text{all}} = Ex + Fu_{\text{pert}} + F_V w \end{cases}$$
(3.2)

- amat_ase Closed-loop A matrix.
- bmat_ase Closed-loop B matrix, from perturbation on the input signals, for all the inputs specified, either used by the controller or not.
- cmat_ase Closed-loop C matrix. From aero-servo-elastic states to y output, which includes the outputs used by the controller, and the input signals returned by the closed-loop controller u_{ctrl} .
- dmat_ase Closed-loop D matrix, input from the controller.
- bvmat_ase Closed-loop B matrix, input from uniform wind in three components, collective, cosine, and sine.
- dvmat_ase Closed-loop D matrix, input from uniform wind.
- bvmat_loc_v_ase Closed-loop B matrix, input from wind at each aerodynamic section along the blade in three components, collective, cosine, and sine.
- dvmat_loc_v_ase Closed-loop D matrix, input from wind at each aerodynamic section along the blade in three components, collective, cosine, and sine.
- emat_ase Closed-loop E matrix. From aero-servo-elastic states to all outputs.
- fmat_ase Closed-loop F matrix. Direct term from perturbation input to all outputs.
- fvmat_ase Closed-loop Fv matrix. Direct term from wind input to all outputs. Wind in three components: collective, cosine, and sine.
- fvmat_loc_v_ase Closed-loop Fv matrix. Direct term from local wind input to all outputs. Wind input for each aerodynamic section along the blade, in the three components: collective, cosine, and sine.

4. Examples

In this chapter a few examples on how to use the program are shown.

4.1. Examples with the GUI: HAWCStab2.exe

In this section a small example on how to use HS2 is shown.

Assuming that no prior calculations are performed, the first thing to calculate is operational points for different wind speeds. When opening the desired htc file under

File->Open HAWC2 model file...

HS2 will produce an error because the *operational_data_filename* file does not exist. This should be ignored by pressing ok on the error dialog box.

4.1.1. Calculating operational points

Normal operation

The first step is to create the operational_data_filename. This is done under

Computation->Optimal operational data

A dialogue box will appear where the user is required to fill various information. If the htc file contains the following

```
begin operational_data ;
windspeed 4.0 25.0 22 ; cut-in [m/s], cut-out [m/s], points [-]
genspeed 300.0 480.0 ; gen. speed. min. [rpm], gen. speed. max. [rpm]
gearratio 50.0 ; [-]
minpitch 0.0 ; [deg.]
opt_lambda 7.5 ; [-]
maxpow 10638.3 ; [kW]
prvs_turbine 1 ; [-] 0 Fixed pitch, 1 PRVS, 2 SRVS
include_torsiondeform 1 ; [-]
end operational_data ;
```

then the default values in the dialogue box are replaced by the values given by the htc file.

Once the computations have been performed the user should save the computed data. This is done under

File->Save optimal power data

The saved data file should be named to match the file name specified by operational_data_filename.

The Gnuplot code found in Listings A.1 has been used to generate Fig. 4.1.



Figure 4.1.: Steady state power and pitch angle values.

Run away operation

For run away stability analysis the operating points are typically calculated for pitch angles of 0 degrees and no generator torque, i.e. max power equal to 0 kW. Furthermore, fixed pitch is selected in the dialog box. The wind speed range being examined is typically from e.g. 8 to 12 m/s with e.g. 9 points. Once these operating points have been found a stability analysis can be performed for the specific operating conditions.

```
begin operational_data ;
windspeed 8.0 12.0 9 ; cut-in [m/s], cut-out [m/s], points [-]
genspeed 300.0 480.0 ; gen. speed. min. [rpm], gen. speed. max. [rpm]
gearratio 50.0 ; [-]
minpitch 0.0 ; [deg.]
opt_lambda 7.5 ; [-]
maxpow 0.0 ; [kW]
prvs_turbine 0 ; [-] 0 Fixed pitch, 1 PRVS, 2 SRVS
include_torsiondeform 1 ; [-]
end operational_data ;
```

4.1.2. Calculating steady state and induction

First ensure that the steps found in Sec. 4.1.1 have been performed. Then

Compute->Steady state and induction

should be chosen. Afterwards further analysis can be performed.

Using

File->Save power...

to produce *def.pwr* provides steady state value for power, pitch angle, blade tip deflections etc. The Gnuplot code found in Listings A.2 has been used to generate Fig. 4.2, where flapwise and edgewise tip deflections are shown.



Figure 4.2.: Steady state blade tip deflections.

Using

File->Save steady state...

to produce multiple files opt_u^* .ind, preferably in a dedicated folder, for various wind speeds provide an extended number of steady state values. The Gnuplot code found in Listings A.3 has been used to generate Fig. 4.3, where the torsion of the blade along the blade span for various wind speed is seen. Steady state pitch values has been added to the total torsion of the blade to get the shown plots.



Figure 4.3.: Steady state blade torsion.

4.1.3. Performing open-loop aeroelastic modal analysis

First, ensure that the steps found in Sec. 4.1.2 have been performed.

Selecting

```
Compute->Structural modal analysis->Entire turbine
```

will compute the structural modes. This calculation is required to perform the

Compute->Aeroelastic modal analysis->Entire turbine

The sort the modes, the following values was used: (0.01,0.30,0.50Hz,0.1,8,sort after mode shapes)

Results obtained from the analysis can be saved under

File->Save modal amplitudes

as e.g. turbine_ae.cmb.

The Gnuplot code found in Listings A.4 and A.5 has been used to generate Fig. 4.4.



Figure 4.4.: Open-loop modal frequencies and damping ratios.

4.1.4. Tuning of PI controller

Selecting

Compute->Tune pitch controller by DTU Wind Energy

A dialogue box will appear where the user is required to fill various information. If the htc file contains the following

begin controller_tuning ;
 partial_load 0.05 0.7; fn [hz], zeta [-]
 full_load 0.06 0.7 ; fn [hz], zeta [-]
 gain_scheduling 1 ; 1 linear, 2 quadratic
 constant_power 1 ; 0 constant torque, 1 constant power
end controller_tuning ;

then the default values in the dialogue box are replaced by the values given by the htc file.

The computations produces *controller_input.txt*, which can be used with the Basic DTU Wind Energy controller [6].

4.1.5. Performing closed-loop aeroelastic modal analysis

To perform a closed-loop analysis several approaches can be used. The first approach is to use one of the two built-in hard coded PI controllers

- basic_dtu_we_controller (# 1)
- pi_pitch_controller (# 2)

where the first can handle full range operation and the second can only handle above rated operation. A description of the parameters is found in Table 2.1, the first two columns in table describe the parameter number for the two controller commands, respectively. Many of the parameters can be calculated by the controller tuning described in Sec. 4.1.4. An example:

pi_pitch_controller 5200 1.2671 0.771100 0.319309 102.68665 754.18745 ... 0.6 0.7 1;

basic_dtu_we_controller 0.19297E+08 0.43304E+07 0.21E+07 1.36516 ...0.669945 11.63317 553.75769 0.6 0.7 1.622 0 ;

Furthermore, the following should be included

```
begin controller ;
begin input ;
constraint bearing1 shaft_rot ;
constraint bearing2 pitch1 collective ;
constraint bearing2 pitch1 cosine ;
constraint bearing2 pitch1 sine ;
end input ;
begin output ;
constraint bearing1 shaft_rot 1 only 2 ; 1
constraint bearing2 pitch1 1 only 1 collective ; 2
constraint bearing2 pitch1 1 only 1 cosine ; 3
constraint bearing2 pitch1 1 only 1 sine ; 4
end output ;
end controller ;
```

The inputs are defining how the wind turbine is controlled. The outputs are defining which sensors the controller is using. The cosine and sine pitch actuators/sensors can be used by an individual pitch controller in the Coleman coordinates.

Additional outputs can be added to the output vector. Those will not be used to close the loop with the controller but they can be used to examine e.g. their transfer functions.

4.2. Examples with the command line program: HS2pid.exe

This program is free but has reduced functionality. Its sole purpose is to provide tuning parameters for a PI controller for the wind turbine. The program is hard coded with blade torsion disabled. If blade torsion is to be included in the analysis HAWC2S.exe is to be used instead.

Procedure for using HS2pid.exe to tune the Basic DTU Wind Energy controller [6].

- The operational parameters should be added to the htc file (sec. 4.1.1).
- The controller data parameters should be added to the htc file (sec. 4.1.4).
- Execute "HS2pid.exe xxx.htc" in a MS-DOS command prompt.
- Use the calculated values from $controller_input.txt$ to tune the controller in the htc file.

The closed loop frequencies should be below the first tower mode. Thus for a floating wind turbine, very low frequencies has to be selected.

5. Keyboard shortcuts

Keys	Action
Shift + x	Rotation about tilt axis
Shift + y	Rotation about yaw axis
Shift + s	Zoom out
Shift + w	Zoom in
Arrow up	Move turbine up (only in turbine view)
Arrow down	Move turbine down (only in turbine view)
Shift + h	Recenter the view
Shift + b	Toggle between blade turbine views
Shift + v	Transparent view
Shift + n	Toggle drawing of nacelle
Shift + a	Decrease amplitude of modal vibration
Shift + q	Increase amplitude of modal vibration
Shift + f	Animate forces due to vibration
Shift + k	Decrease speed of modal vibration
Shift + i	Increase speed of modal vibration
Shift + c	Draw aerodyn. choord. sys.
Shift + e	Draw struct. choord. sys.

Appendix A.

GnuPlot files

Listing A.1: Gnuplot commands used to power and pitch figure.

Listing A.2: Gnuplot commands used to deflection figure.

```
reset
set term post eps soli mono 12
set out 'deflec.eps
set key right
set size 0.4,0.4
set xr [3:25]
#set yr [0:11]
set format y '%3g'
set xlabel 'Wind speed [m/s]'
set ylabel 'Blade tip deflection [m]'
plot 'def.pwr' us 1:($12+3.766) t 'Flapwise' w lp pt 7 lt 7, \
        'def.pwr' us 1:($11) t 'Edgewise' w lp pt 5 lt 7
set term wxt
set out
```



```
reset
set term post eps soli mono 12
set out 'torsion.eps'
set key left bottom
set size 0.4,0.32
set xr [0:90]
#set yr [-1.5:2]
set format y '%3g'
set xlabel 'Blade curve coord. [m]'
```

Listing A.4: Gnuplot commands used to generate modal frequencies figure.

```
reset
set term post eps soli mono 12
set out 'turbine_frq.eps'
set key at 24,0.6
set size 0.4,0.8
set xr [4:25]
set yr [0.2:1.2]
set format y '%3g'
set xlabel 'Wind speed [m/s]'
set ylabel 'Modal frequencies [Hz]'
plot 'turbine_ae.cmb' us 1:2 t 'Lat. twr' w lp pt 1 lt 7, \setminus
     'turbine_ae.cmb' us 1:3 t 'Long. twr' w lp pt 2 lt 7, \setminus
   'turbine_ae.cmb' us 1:4 t 'B.W. flap' w lp pt 3 lt 7, \setminus
     'turbine_ae.cmb' us 1:5 t 'DT tors.' w lp pt 4 lt 7, \setminus
     'turbine_ae.cmb' us 1:6 t 'Sym. flap' w lp pt 5 lt 7,
     'turbine_ae.cmb' us 1:7 t 'F.W. flap' w lp pt 6 lt 7, \setminus
     'turbine_ae.cmb' us 1:8 t 'B.W. edge' w lp pt 7 lt 7, \setminus
     'turbine_ae.cmb' us 1:9 t 'F.W. edge' w lp pt 8 lt 7
set term wxt
set out
```

Listing A.5: Gnuplot commands used to generate modal damping ratios figure.

```
reset
set term post eps soli mono 12
set out 'turbine_dmp.eps'
set xr [4:25]
set multiplot
set size 0.4,0.39
set orig 0,0.42
set format × '%g'
set format y '%3.0f'
set xlabel ''
set xlabel
set yr [40:100]
set ytics 40,20,100
set ylabel 'Damping ratio [%]'
set key at 24,60
<code>plot</code> <code>'turbine_ae.cmb'</code> us 1:12 t <code>'B.W.</code> flap' w lp pt 3 lt 7, \setminus
       'turbine_ae.cmb' us 1:14 t 'Sym. flap' w lp pt 5 lt 7, \backslash 'turbine_ae.cmb' us 1:15 t 'F.W. flap' w lp pt 6 lt 7
set size 0.4,0.39
```

```
set orig 0,0
set format x '%g'
set format y '%3.0f'
set xlabel 'Wind speed [m/s]'
set ylabel 'Damping ratio [%]'
set key at 24,8
set ytics 0,2,12
set yr [0:12]
plot 'turbine_ae.cmb' us 1:10 t 'Lat. twr' w lp pt 1 lt 7, \
        'turbine_ae.cmb' us 1:11 t 'Long. twr' w lp pt 2 lt 7, \
        'turbine_ae.cmb' us 1:13 t 'DT tors.' w lp pt 4 lt 7, \
        'turbine_ae.cmb' us 1:16 t 'B.W. edge' w lp pt 7 lt 7, \
        'turbine_ae.cmb' us 1:17 t 'F.W. edge' w lp pt 8 lt 7
unset multiplot
set term wxt
set out
```

Bibliography

- Hansen MH. Aeroelastic stability analysis of wind turbines using an eigenvalue approach. Wind Energy 2004; 7(2):133-143, doi:10.1002/we.116.
- [2] Hansen MH. Aeroelastic properties of backward swept blades. 49th AIAA Aerospace Sciences Meeting including the New Horizons Forum and Aerospace Exposition. American Institute of Aeronautics and Astronautics, 2011, doi:10.2514/6.2011-260.
- [3] Sønderby I, Hansen MH. Open-loop frequency response analysis of a wind turbine using a high-order linear aeroelastic model. Wind Energy 2014; 17: 1147–1167, doi: 10.1002/we.1624.
- [4] Larsen TJ, Hansen MA. How 2 HAWC2, the user's manual. Technical Report Risø-R-1597(ver. 3-1)(EN), Risø National Laboratory, 2007. www.hawc2.dk
- [5] Hansen MH. Anisotropic damping of Timoshenko beam elements. Technical Report Risø-R-1267(EN), Risø National Laboratory, Denmark, 2001.
- [6] Hansen MH, Henriksen LC. Basic DTU Wind Energy controller. *Technical Report* E-0028, DTU Wind Energy, 2013.
- [7] Tibaldi C, Henriksen LC, Hansen MH, Bak C. Effects of gain-scheduling methods in a classical wind turbine controller on wind turbine aero-servo-elastic modes and loads. 32nd ASME Wind Energy Symposium. American Institute of Aeronautics and Astronautics, 2014, doi:10.2514/6.2014-0873.